

§16.4 Divergence, Curl, Green's Theorem

Useful notation: $\nabla = \left\langle \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right\rangle$

So if $f(x, y, z)$ is a function of three variables, $\nabla f = \left\langle \frac{\partial}{\partial x}(f), \frac{\partial}{\partial y}(f), \frac{\partial}{\partial z}(f) \right\rangle$

If $\mathbf{F}(x, y, z) = P(x, y, z)\mathbf{i} + Q(x, y, z)\mathbf{j} + R(x, y, z)\mathbf{k}$ is a vector field:

$$\bullet \nabla \cdot \mathbf{F} = \left\langle \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right\rangle \cdot \langle P, Q, R \rangle = \frac{\partial}{\partial x} P + \frac{\partial}{\partial y} Q + \frac{\partial}{\partial z} R$$

$$\leadsto \nabla \cdot \mathbf{F} = P_x + Q_y + R_z \quad (\text{called } \operatorname{div}(\mathbf{F}))$$

$$\bullet \nabla \times \mathbf{F} =$$

$$\left\langle \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right\rangle \times \langle P, Q, R \rangle$$

Here \bullet and \times are being "slightly abused notation"

$$= \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ P & Q & R \end{vmatrix} = \hat{i} \left(\frac{\partial}{\partial y} R - \frac{\partial}{\partial z} Q \right) - \hat{j} \left(\frac{\partial}{\partial x} R - \frac{\partial}{\partial z} P \right) + \hat{k} \left(\frac{\partial}{\partial x} Q - \frac{\partial}{\partial y} P \right)$$

$$= \langle R_y - Q_z, P_z - R_x, Q_x - P_y \rangle = \operatorname{curl}(\mathbf{F})$$

(From §16.3)

Ex. Find $\operatorname{div}(\mathbf{F})$ & $\operatorname{curl}(\mathbf{F})$, $\mathbf{F} = \langle xy, 2y^2, x+z \rangle$

$$\operatorname{div} \mathbf{F} = P_x + Q_y + R_z = y + 4y + 1 = \boxed{5y+1}$$

$$\operatorname{curl} \mathbf{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ xy & 2y^2 & x+z \end{vmatrix} = \langle 0-0, -(1-0), 0-x \rangle$$

$$= \boxed{\langle 0, -1, -x \rangle}$$

How do we measure the change of a vector field?

1. Curl (in \mathbb{R}^3)

↙ Cross product only
defined for vectors in \mathbb{R}^3

- Tells us Flow / Circulation density
- Measures local circulation at a point
- Is a vector
- Direction gives axis of rotation (using right hand rule)
- Magnitude gives rotation rate
- $\text{curl } \mathbf{F} = \nabla \times \mathbf{F}$
- If $\mathbf{F} = P\mathbf{i} + Q\mathbf{j}$: we use $\nabla \times \mathbf{F} = \nabla \times \langle P, Q, 0 \rangle = \langle 0, 0, Q_x - P_y \rangle$

⊕ From §16.3 THM:
 $\text{Curl}(\mathbf{F}) = \langle 0, 0, 0 \rangle \iff \mathbf{F}$ is conservative
 (ie. $\mathbf{F} = \nabla f$ for some $f: \mathbb{R}^3 \rightarrow \mathbb{R}$)

Geometric meaning $\text{Curl}(\mathbf{F}) = \vec{0}$ is "F has no rotation"

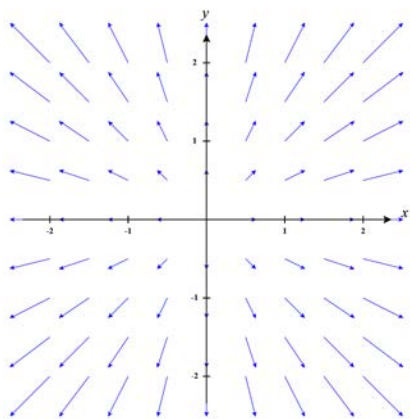
2. Divergence (in any \mathbb{R}^n)

- Tells us Flux density
- Measures Compression/expansion at a point
- Is a Scalar
- $\text{div } \mathbf{F} = \nabla \cdot \mathbf{F}$

THM: $\text{div } \mathbf{F} = \vec{0} \implies \mathbf{F} = \nabla \times \mathbf{G}$
 for some other vector field \mathbf{G} .

Geometric meaning to $\text{div } \mathbf{F} = \vec{0}$ is \mathbf{F} is
 "incompressible" or "no expansion/compression"

Example 138. Let $\mathbf{F}(x, y) = \langle x, y \rangle$. Based on the visualization of this vector field below, what can we say about the sign (+, -, 0) of the divergence and scalar curl of this vector field? Verify by computing the divergence and scalar curl.

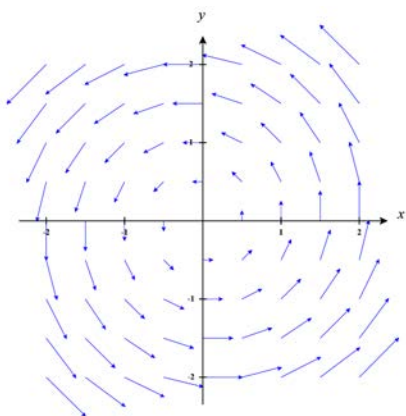


lots of expansion, so $\text{div}(\mathbf{F})$ should be positive at every point. (and $\text{Flux} = \oint_C \mathbf{F} \cdot \mathbf{n} \, ds > 0$)

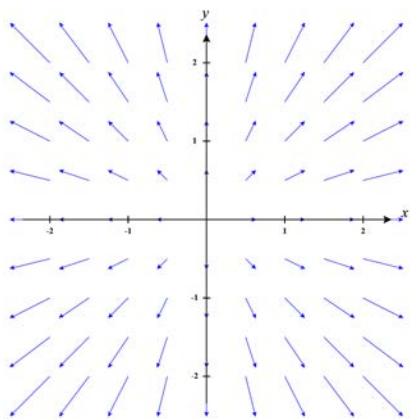
no rotation, so $\text{curl}(\mathbf{F})$ should be the zero vector.
(and $\mathbf{F} = \nabla f$ & $\text{Flow} = \oint_C \mathbf{F} \cdot \mathbf{T} \, ds = f(\mathbf{A}) - f(\mathbf{A}) = 0$)

Check: $\text{div } \mathbf{F} = P_x + Q_y = 1 + 1 = 2 \checkmark$
 $\text{curl } \mathbf{F} = \langle 0, 0, Q_x - P_y \rangle = \langle 0, 0, 0 - 0 \rangle$
 $= \langle 0, 0, 0 \rangle \checkmark$

Example 139. *You try it!* Let $\mathbf{F}(x, y) = \langle -y, x \rangle$. Based on the visualization of this vector field below, what can we say about the sign (+, -, 0) of the divergence and scalar curl of this vector field? Verify by computing the divergence and scalar curl.



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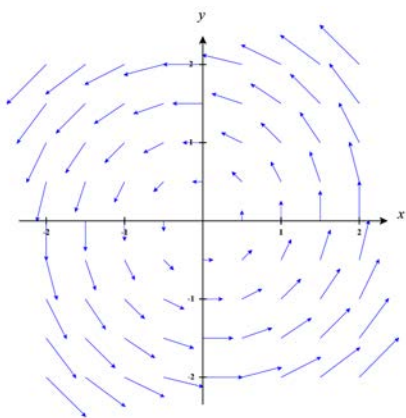


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 $= \langle 0, 0, 0 \rangle \checkmark$

Example 139. *You try it!* Let $\mathbf{F}(x, y) = \langle -y, x \rangle$. Based on the visualization of this vector field below, what can we say about the sign (+, -, 0) of the divergence and scalar curl of this vector field? Verify by computing the divergence and scalar curl.



lots of rotation so $\text{curl}(\mathbf{F}) \neq \vec{0}$
and should be pointing "up"
out of the page by RHR

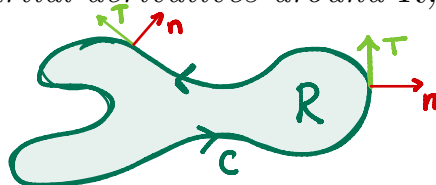
No compression, so $\text{div}(\mathbf{F}) = 0$

Check $\text{curl } \mathbf{F} = \langle 0, 0, Q_x - P_y \rangle$
 $= \langle 0, 0, 1 - (-1) \rangle = \langle 0, 0, 2 \rangle$ "up" \checkmark
 $\text{div } \mathbf{F} = P_x + Q_y = 0 + 0 = 0 \checkmark$

Question: How is this useful?

Answer: We can relate rates of change of F inside a region to the behavior of the vector field on the boundary of the region.

Theorem 140 (Green's Theorem). Suppose C is a piecewise smooth, simple, closed curve enclosing on its left a region R in the plane with outward oriented unit normal \mathbf{n} . If $\mathbf{F} = \langle P, Q \rangle$ has continuous partial derivatives around R , then



a) Circulation form:

$$(a) \quad \int_C \mathbf{F} \cdot \mathbf{T} \, ds = \int_C P \, dx + Q \, dy = \iint_R (\nabla \times \mathbf{F}) \cdot \mathbf{k} \, dA = \iint_R Q_x - P_y \, dA$$

b) Flux form:

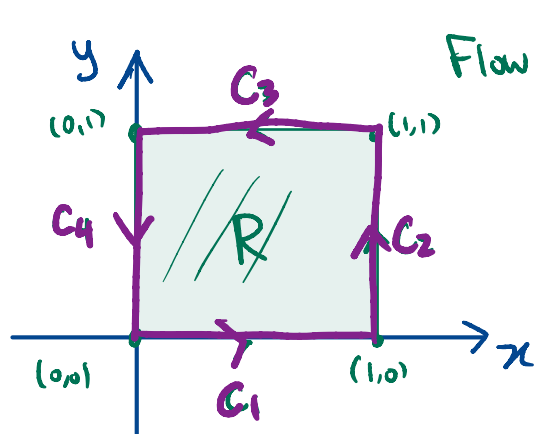
$$(b) \quad \int_C \mathbf{F} \cdot \mathbf{n} \, ds = \int_C P \, dy - Q \, dx = \iint_R (\nabla \cdot \mathbf{F}) \, dA = \iint_R P_x + Q_y \, dA$$

\uparrow notational equality \uparrow G's T \uparrow expand out $(\nabla \times \mathbf{F}) \cdot \hat{\mathbf{k}}$ or $\nabla \cdot \mathbf{F}$

(a) Says: The Flow across a closed simple loop C is the double-integral over the interior R of C of the $\hat{\mathbf{k}}$ -component of $\text{Curl } \mathbf{F}$.

(b) Says: The Flux across a closed simple loop C is the double-integral of the interior R of C of $\text{div } \mathbf{F}$

Example 141. Evaluate the line integral $\int_C \mathbf{F} \cdot \mathbf{T} \, ds$ for the vector field $\mathbf{F} = \langle -y^2, xy \rangle$ where C is the boundary of the square bounded by $x = 0, x = 1, y = 0$, and $y = 1$ oriented counterclockwise. *$C = C_1 \cup C_2 \cup C_3 \cup C_4$ yuck!*



$$\text{Flow} = \oint_C \mathbf{F} \cdot \mathbf{T} \, ds = \int_{C_1} \mathbf{F} \cdot d\mathbf{r} + \int_{C_2} \mathbf{F} \cdot d\mathbf{r} + \int_{C_3} \mathbf{F} \cdot d\mathbf{r} + \int_{C_4} \mathbf{F} \cdot d\mathbf{r}$$

or use G'sT

$$\oint \mathbf{F} \cdot \mathbf{T} \, ds = \iint_R \text{curl} \mathbf{F} \cdot \hat{\mathbf{k}} \, dA$$

$$= \iint_R Q_x - P_y \, dA = \iint_R y - (-2y) \, dA$$

better!

$$= \int_0^1 \int_0^1 3y \, dy \, dx = \int_0^1 \left. \frac{3}{2} y^2 \right|_0^1 dx = \int_0^1 \frac{3}{2} dx$$

$$= \left. \frac{3}{2} x \right|_0^1 = \frac{3}{2} (1 - 0) = \boxed{\frac{3}{2}}$$

Example 142. Compute the flux out of the region R which is the portion of the annulus between the circles of radius 1 and 3 in the first ^{quadrant} for the vector field $\mathbf{F} = \langle \frac{1}{3}x^3, \frac{1}{3}y^3 \rangle$.

$$\text{Flux} = \oint_C \mathbf{F} \cdot \mathbf{n} \, ds \stackrel{\text{G'sT}}{=} \iint_R P_x + Q_y \, dA$$

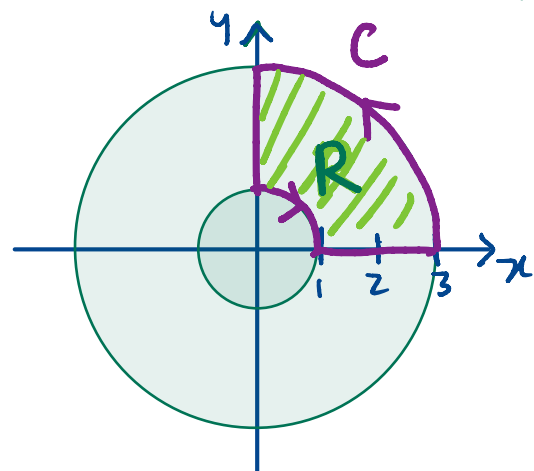
$$= \iint_R x^2 + y^2 \, dA$$

*polar coord.
 $x^2 + y^2 = r^2$*

$$\stackrel{\text{polar coord.}}{=} \int_0^{\pi/2} \int_1^3 r^2 \cdot r \, dr \, d\theta = \int_0^{\pi/2} \int_1^3 r^3 \, dr \, d\theta$$

$$= \int_0^{\pi/2} \left. \frac{1}{4} r^4 \right|_1^3 d\theta = \int_0^{\pi/2} \frac{81}{4} - \frac{1}{4} d\theta = 20\theta \Big|_0^{\pi/2} = 20 \cdot \frac{\pi}{2}$$

$$= \boxed{10\pi}$$



Example 143. Let R be the region bounded by the curve $\mathbf{r}(t) = \langle \sin(2t), \sin(t) \rangle$ for $0 \leq t \leq \pi$. Find the area of R , using Green's Theorem applied to the vector field

⊗ $\mathbf{F} = \frac{1}{2} \langle x, y \rangle$

For Flux

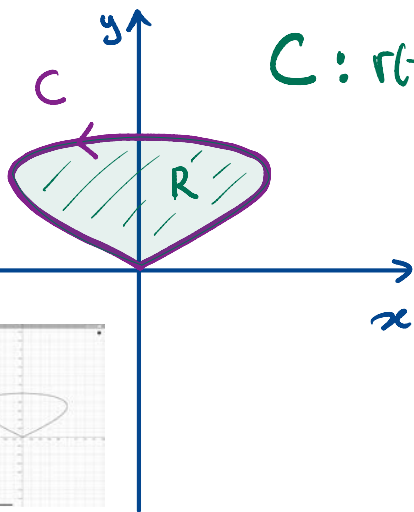
or $\mathbf{F} = \langle -\frac{1}{2}y, \frac{1}{2}x \rangle$

For Flow

Idea: $\text{Area } R = \iint_R 1 \, dA = \iint_R \frac{1}{2} - (-\frac{1}{2}) \, dA$

G'sT(Flow)

$= \oint_C \mathbf{F} \cdot \mathbf{T} \, ds$ w/ $\mathbf{F} = \langle -\frac{1}{2}y, \frac{1}{2}x \rangle$



$C: \mathbf{r}(t) = \langle \sin 2t, \sin t \rangle \quad \mathbf{r}'(t) = \langle 2\cos 2t, \cos t \rangle$
 $t \in [0, \pi]$

$\text{Area } R = \oint_C \langle -\frac{1}{2}y, \frac{1}{2}x \rangle \cdot \mathbf{T} \, ds$

$= \int_0^\pi \langle -\frac{1}{2} \sin t, \frac{1}{2} \sin 2t \rangle \cdot \langle 2\cos 2t, \cos t \rangle \, ds$

$= \int_0^\pi -\sin t \cos 2t + \frac{1}{2} \sin 2t \cos t \, dt$

Unclear how to integrate?

$\cos 2t = 2\cos^2 t - 1$

$\sin 2t = 2\sin t \cos t$

$= \int_0^\pi -\sin t (2\cos^2 t - 1) + \frac{1}{2} (2\sin t \cos t) \cos t \, dt$

$= \int_0^\pi -2\cos^2 t \sin t + \sin t + \sin t \cos^2 t \, dt$

u-sub
 $u = \cos t$
 $du = -\sin t \, dt$

⊗ Same

$= \int_0^\pi -\cos^2 t \sin t + \sin t \, dt = \left[\frac{1}{3} \cos^3 t - \cos t \right]_0^\pi = \left[\frac{1}{3} (\cos \pi)^3 - \cos \pi \right] - \left[\frac{1}{3} (\cos 0)^3 - \cos 0 \right]$

$= \frac{2}{3} + \frac{2}{3} = \boxed{\frac{4}{3}}$

Note: This is the idea behind the operation of the measuring instrument known as a planimeter.

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⊗ $\mathbf{F} = \frac{1}{2} \langle x, y \rangle$

For Flux

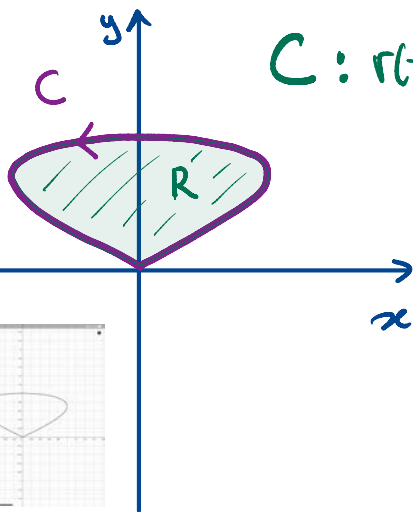
or $\mathbf{F} = \langle -\frac{1}{2}y, \frac{1}{2}x \rangle$

For Flow

Idea: $\text{Area } R = \iint_R 1 \, dA = \iint_R \frac{1}{2} + \frac{1}{2} \, dA$

G'sT(Flux)

$= \oint_C \mathbf{F} \cdot \mathbf{n} \, ds$ w/ $\mathbf{F} = \langle \frac{1}{2}x, \frac{1}{2}y \rangle$



$C: \mathbf{r}(t) = \langle \sin 2t, \sin t \rangle$
 $t \in [0, \pi]$

$\mathbf{r}'(t) = \langle 2\cos 2t, \cos t \rangle$

$\mathbf{n} \sim \langle \cos t, -2\cos 2t \rangle$

$\text{Area } R = \oint_C \langle \frac{1}{2}x, \frac{1}{2}y \rangle \cdot \mathbf{n} \, ds$

$= \int_0^\pi \langle \frac{1}{2}\sin 2t, \frac{1}{2}\sin t \rangle \cdot \langle \cos t, -2\cos 2t \rangle \, ds$

$= \int_0^\pi \frac{1}{2} \sin 2t \cos t - \sin t \cos 2t \, dt$

Unclear how to integrate?

$\cos 2t = 2\cos^2 t - 1$

$\sin 2t = 2\sin t \cos t$

$= \int_0^\pi \frac{1}{2} (2\sin t \cos t) \cos t - \sin t (2\cos^2 t - 1) \, dt$

$= \int_0^\pi \cos^2 t \sin t - 2\cos^2 t \sin t + \sin t \, dt$

u-sub
 $u = \cos t$
 $du = -\sin t \, dt$

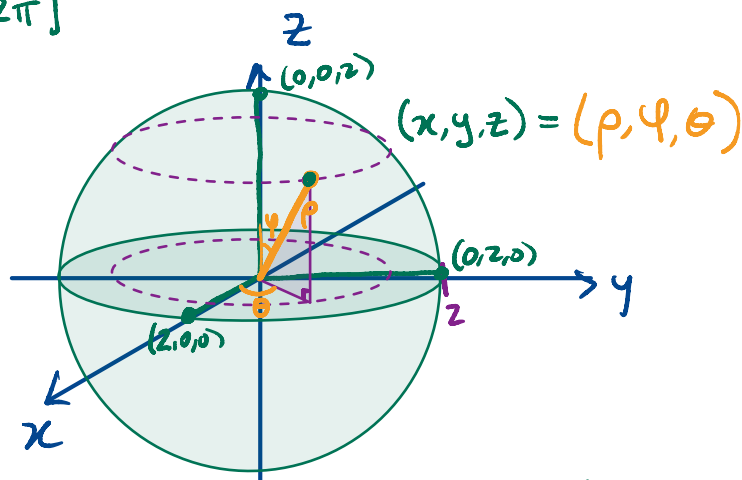
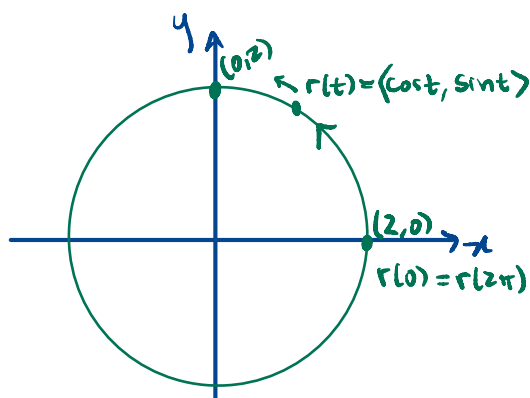
⊗ same
 $= \int_0^\pi -\cos^2 t \sin t + \sin t \, dt = \frac{1}{3} \cos^3 t - \cos t \Big|_0^\pi = \left[\frac{1}{3} (\cos \pi)^3 - \cos \pi \right] - \left[\frac{1}{3} (\cos 0)^3 - \cos 0 \right]$
 $= \frac{2}{3} + \frac{2}{3} = \boxed{\frac{4}{3}}$

Note: This is the idea behind the operation of the measuring instrument known as a planimeter.

§16.5, 16.6 Surfaces & Surface Integrals

Different ways to think about curves and surfaces:

| | Curves | Surfaces |
|------------------|---|---|
| Explicit: | $y = f(x)$ | $z = f(x, y)$ |
| | $y = \sqrt{4 - x^2}$ | $z = \sqrt{4 - x^2 - y^2}$ |
| Implicit: | $F(x, y) = 0$ | $F(x, y, z) = 0$ |
| | $x^2 + y^2 = 4$ | $x^2 + y^2 + z^2 = 4$ |
| Parametric Form: | $\mathbf{r}(t) = \langle x(t), y(t) \rangle$ | $\vec{r}(s, t) = \langle x(s, t), y(s, t), z(s, t) \rangle$ |
| | $\mathbf{r}(t) = \langle 2 \cos t, 2 \sin t \rangle$ $t \in [0, 2\pi]$ | |



We've already done a few
Surface parametrizations.

e.g.

⊕ Plane through the origin

$$\mathbf{r}(s, t) = s\vec{v}_1 + t\vec{v}_2$$

⊕ Spheres w/ fixed radius ρ
using spherical coords

Sphere of
radius $\rho = 2$

$$x = \rho \sin \varphi \cos \theta$$

$$y = \rho \sin \varphi \sin \theta$$

$$z = \rho \cos \varphi$$

$$\text{So } \vec{r}(s, t) = \langle 2 \sin(s) \cos(t), 2 \sin(s) \sin(t), 2 \cos(s) \rangle$$

or can just call parameters φ, θ , so

$$\vec{r}(\varphi, \theta) = \langle 2 \sin \varphi \cos \theta, 2 \sin \varphi \sin \theta, 2 \cos \varphi \rangle$$



GOAL: $r: \mathbb{R}^2 \rightarrow \mathbb{R}^3$ such that range of r is surface.

Example 144. Give parametric representations for the surfaces below.

given x as a function of y & z so set $y=s$ & $z=t$ the parameters.

a) $x = y^2 + \frac{1}{2}z^2 - 2$ ①

$$\vec{r}(s,t) = \langle s^2 + \frac{1}{2}t^2 - 2, s, t \rangle$$

$s \in \mathbb{R}, t \in \mathbb{R}$

Can also swap roles of s and t

$$\vec{r}(s,t) = \langle t^2 + \frac{1}{2}s^2 - 2, t, s \rangle$$

$s, t \in \mathbb{R}$

Or can try something like

$$\begin{cases} y = r \cos \theta \\ z = \sqrt{2} r \sin \theta \end{cases} \text{ then } y^2 + \frac{1}{2}z^2 = r^2$$

so $x = r^2 - 2$

$$\vec{r}(r,\theta) = \langle r^2 - 2, r \cos \theta, \sqrt{2} r \sin \theta \rangle$$

$r \geq 0, \theta \in [0, 2\pi]$

①, ②, ③ all are parametrizations of the surface for (a).

b) The portion of the surface $x = y^2 + \frac{1}{2}z^2 - 2$ which lies behind the yz -plane.

Same \vec{r} w/ new ranges for s, t . (x, y, z) is behind yz -plane if $x \leq 0$

So need $x = y^2 + \frac{1}{2}z^2 - 2 \leq 0$

$\Rightarrow y^2 + \frac{1}{2}z^2 \leq 2$ (ellipse) for ① & ②

c) $x^2 + y^2 + z^2 = 9$

$\Rightarrow \frac{y^2}{2} + \frac{z^2}{4} \leq 1$ and

$$\begin{cases} y \in [-\sqrt{2}, \sqrt{2}] \\ z \in [-\sqrt{4-2y^2}, \sqrt{4-2y^2}] \end{cases}$$

or just need $r^2 - 2 \leq 0$ so $r \leq \sqrt{2}$ for ③

$$\begin{cases} r \in [0, \sqrt{2}] \\ \theta \in [0, 2\pi] \end{cases}$$

Sphere of radius $\rho = 3$.

Spherical coords.

@ $\rho = 3$ $\begin{cases} x = \rho \sin \varphi \cos \theta \\ y = \rho \sin \varphi \sin \theta \\ z = \rho \cos \varphi \end{cases}$

$$\vec{r}(\varphi, \theta) = \langle 3 \sin \varphi \cos \theta, 3 \sin \varphi \sin \theta, 3 \cos \varphi \rangle$$

$\varphi \in [0, \pi], \theta \in [0, 2\pi]$

Cartesian coords

$$x \in [-3, 3]$$

$$y \in [-\sqrt{9-x^2}, \sqrt{9-x^2}]$$

$$z = \sqrt{9-x^2-y^2} \text{ (top half only!)}$$

$$\vec{r}(s,t) = \langle s, t, \sqrt{9-s^2-t^2} \rangle$$

$s \in [-3, 3], t \in [-\sqrt{9-s^2}, \sqrt{9-s^2}]$

d) $x^2 + y^2 = 25$

cylinder w/ horizontal cross-sections of radius $r = 5$.

Cylindrical coords

@ $r = 5$ $\begin{cases} x = r \cos \theta \\ y = r \sin \theta \\ z = z \end{cases}$

$$\vec{r}(\theta, t) = \langle 5 \cos \theta, 5 \sin \theta, t \rangle$$

$\theta \in [0, 2\pi], t \in \mathbb{R}$

Can try cartesian?

$$x \in [-5, 5]$$

$$y = \sqrt{25-x^2} \text{ (right half only)}$$

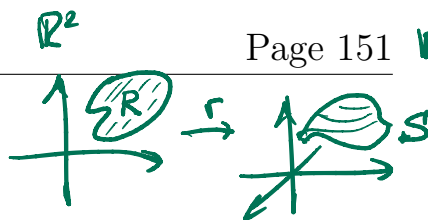
$$z = z$$

$$\vec{r}(s,t) = \langle s, \sqrt{25-s^2}, t \rangle$$

$s \in [-5, 5], t \in \mathbb{R}$

What can we do with this?

Surface area

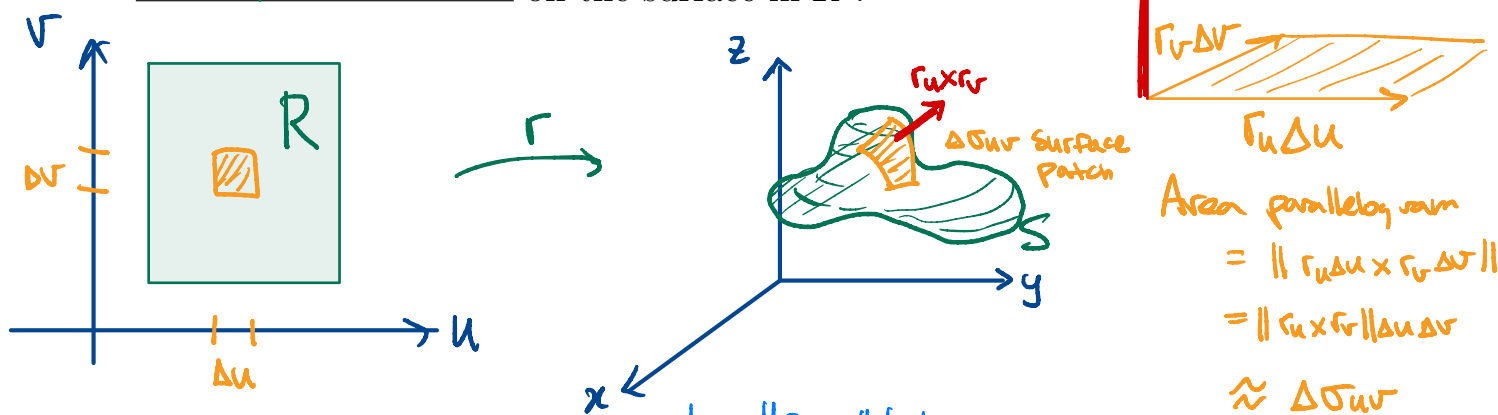


If our parameterization is **smooth** ($\mathbf{r}_u, \mathbf{r}_v$ not parallel in the domain), then:

- $\mathbf{r}_u \times \mathbf{r}_v$ is normal to the surface $S: \mathbf{r}(u,v) = \langle x(u,v), y(u,v), z(u,v) \rangle$
 $u, v \in R$

- A rectangle of size $\Delta u \times \Delta v$ in the uv -domain is mapped to a rectangle of size

$\|\mathbf{r}_u \times \mathbf{r}_v\| \Delta u \Delta v$ on the surface in \mathbb{R}^3 .



- Thus, $\text{Area}(S) =$

$$\iint_S 1 \, d\sigma = \iint_R \|\mathbf{r}_u \times \mathbf{r}_v\| \, dA$$

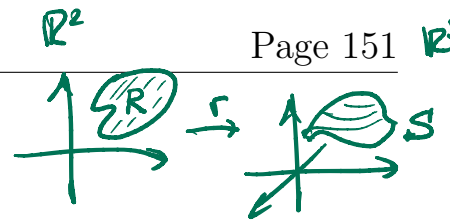
$d\sigma = \|\mathbf{r}_u \times \mathbf{r}_v\| \, du \, dv$
 Surface integral w/ surface measure $d\sigma$

$dA = du \, dv = r \, dr \, d\theta$ etc
 double integral w/ Area measure

Example 145. *You try it!* Find the area of the portion of the cylinder $x^2 + y^2 = 25$ between $z = 0$ and $z = 1$.

What can we do with this?

Surface area

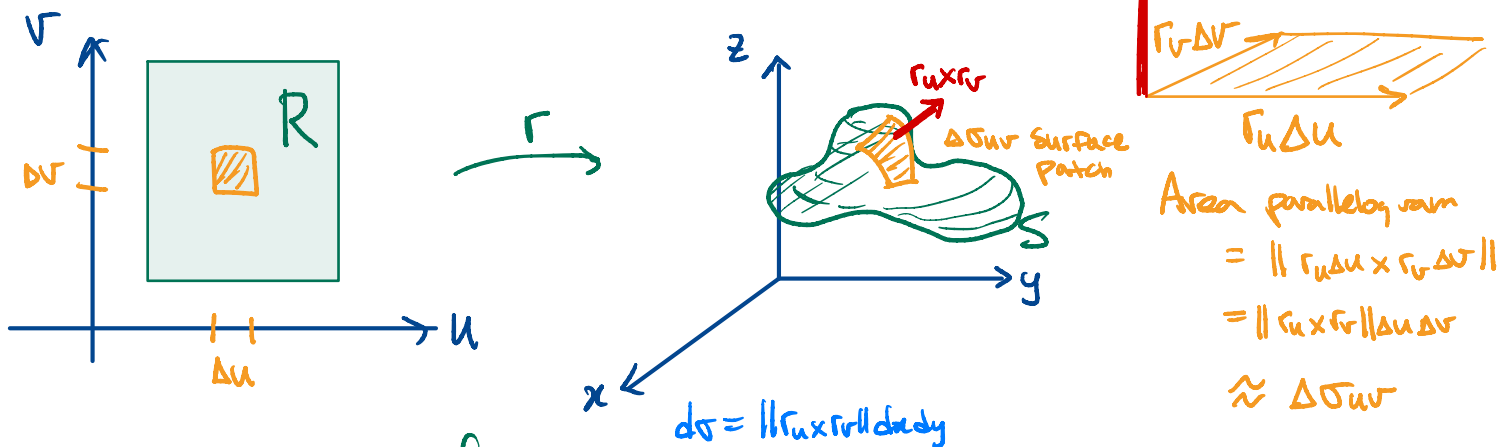


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 $u, v \in R$

- A rectangle of size $\Delta u \times \Delta v$ in the uv -domain is mapped to a rectangle of size

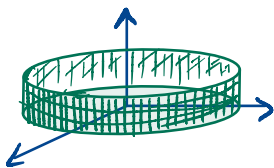
$\|\mathbf{r}_u \times \mathbf{r}_v\| \Delta u \Delta v$ on the surface in \mathbb{R}^3 .



- Thus, $\text{Area}(S) = \iint_S 1 d\sigma = \iint_R \|\mathbf{r}_u \times \mathbf{r}_v\| dA$
 $d\sigma = \|\mathbf{r}_u \times \mathbf{r}_v\| du dv$
 $dA = du dv = r dr d\theta$ etc
 Surface integral w/ surface measure $d\sigma$
 double integral w/ Area measure

Example 145. *You try it!* Find the area of the portion of the cylinder $x^2 + y^2 = 25$

between $z = 0$ and $z = 1$.



$$\vec{r}(\theta, t) = \langle 5 \cos \theta, 5 \sin \theta, t \rangle, \quad \theta \in [0, 2\pi], \quad z \in [0, 1]$$

$$\vec{r}_\theta = \langle -5 \sin \theta, 5 \cos \theta, 0 \rangle$$

$$\vec{r}_t = \langle 0, 0, 1 \rangle$$

$$\text{So } \mathbf{n} = \mathbf{r}_\theta \times \mathbf{r}_t = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ -5 \sin \theta & 5 \cos \theta & 0 \\ 0 & 0 & 1 \end{vmatrix} = \langle 5 \cos \theta, -(-5 \sin \theta), 0 \rangle$$

$$\text{So } \|\mathbf{n}\|^2 = 25 \cos^2 \theta + 25 \sin^2 \theta + 0 = 25, \quad \|\mathbf{n}\| = 5.$$

$$\text{Area } S = \iint_R 5 dA = \int_0^{2\pi} \int_0^1 5 dt d\theta = \int_0^{2\pi} 5t \Big|_0^1 d\theta = \int_0^{2\pi} 5 d\theta = 5 \cdot 2\pi = 10\pi$$

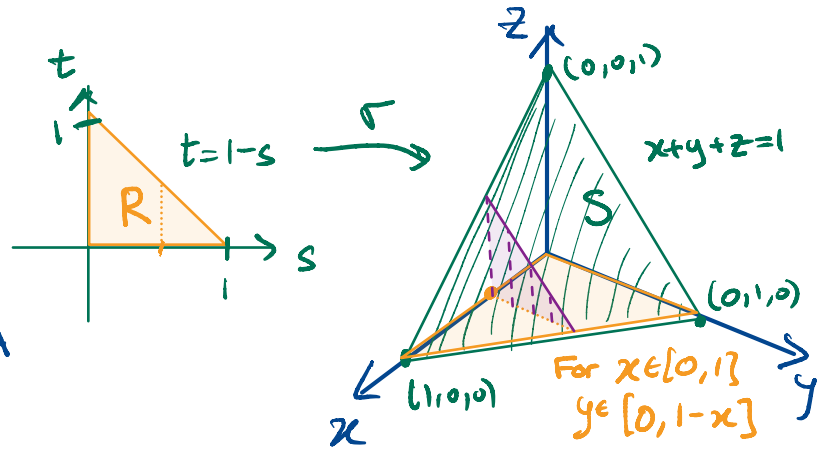
Example 146. Suppose the density of a thin plate S in the shape of the portion of the plane $x + y + z = 1$ in the first octant is $\delta(x, y, z) = 6xy$. Find the mass of the plate.

$$M = \iint_S \delta(x, y, z) \, d\sigma$$

Step 1: parametrize S

Step 2: Compute $d\sigma = \|\mathbf{r}_s \times \mathbf{r}_t\| \, dA$

Step 3: Substitute



$$x \in [0, 1]$$

$$y \in [0, 1-x]$$

$$\text{Then } z = 1 - x - y$$

Step 1:

$$\mathbf{r}(s, t) = \langle s, t, 1-s-t \rangle$$

$$R: s \in [0, 1], t \in [0, 1-s]$$

$$\text{Step 2: } \mathbf{r}_s = \langle 1, 0, -1 \rangle$$

$$\mathbf{r}_t = \langle 0, 1, -1 \rangle$$

$$\mathbf{r}_s \times \mathbf{r}_t = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ 1 & 0 & -1 \\ 0 & 1 & -1 \end{vmatrix}$$

$$= \langle 1, -(-1), 1 \rangle$$

$$= \langle 1, 1, 1 \rangle \text{ so } \|\mathbf{r}_s \times \mathbf{r}_t\| = \sqrt{3}$$

Step 3:

$$\text{Mass} = \iint_S \delta \, d\sigma = \iint_R 6xy \sqrt{3} \, dA = \int_0^1 \int_0^{1-s} 6\sqrt{3} \, st \, dt \, ds$$

$$= \int_0^1 3\sqrt{3} st^2 \Big|_0^{1-s} ds = \int_0^1 3\sqrt{3} s (1-s)^2 ds = \int_0^1 3\sqrt{3} s (s^2 - 2s + 1) ds$$

$$= \int_0^1 3\sqrt{3} (s^3 - 2s^2 + s) ds = 3\sqrt{3} \left(\frac{1}{4} s^4 - \frac{2}{3} s^3 + \frac{1}{2} s^2 \right) \Big|_0^1 = 3\sqrt{3} \left(\frac{1}{4} - \frac{2}{3} + \frac{1}{2} \right) - 0$$

$$= 3\sqrt{3} \left(\frac{3}{4} - \frac{2}{3} \right) = 3\sqrt{3} \left(\frac{9-8}{12} \right) = \frac{3\sqrt{3}}{12} = \frac{\sqrt{3}}{4}$$

$$\boxed{\frac{\sqrt{3}}{4}}$$

§16.6, 16.7 Flux Surface Integrals, Stokes' Theorem

Goal: If \mathbf{F} is a vector field in \mathbb{R}^3 , find the total flux of \mathbf{F} through a surface S .

Note: If the flux is positive, that means the net movement of the field through S is in the direction of the outward pointing normal vector of S

(as chosen in the orientation of S)

If $\mathbf{r}(u, v)$ is a smooth parameterization of S with domain R , we have

$$\text{flux of } \mathbf{F} \text{ through } S = \iint_S (\mathbf{F} \cdot \mathbf{n}) \, d\sigma = \iint_R \mathbf{F}(\mathbf{r}(u, v)) \cdot (\mathbf{r}_u \times \mathbf{r}_v) \, dA.$$

\nwarrow unit normal \nwarrow plug in parametrization into \mathbf{F}

$\tilde{\mathbf{n}} = \frac{\mathbf{r}_u \times \mathbf{r}_v}{\|\mathbf{r}_u \times \mathbf{r}_v\|}$ so \uparrow is $n * \|\mathbf{r}_u \times \mathbf{r}_v\|$.

Example 147. Find $\mathbf{r}_u \times \mathbf{r}_v$ and $\|\mathbf{r}_u \times \mathbf{r}_v\|$ when $z = f(x, y)$ so that S is the graph of a scalar function with domain in \mathbb{R}^2 .

Example 148. Find $\mathbf{r}_u \times \mathbf{r}_v$ and $\|\mathbf{r}_u \times \mathbf{r}_v\|$ when S is a portion of a sphere of radius $\rho = a$, for some fixed constant a , using the standard spherical coordinates for your parametrization.

Soln. $\mathbf{r}_\varphi = \langle a \cos \varphi \cos \theta, a \cos \varphi \sin \theta, -a \sin \varphi \rangle$

$\mathbf{r}_\theta = \langle -a \sin \varphi \sin \theta, a \sin \varphi \cos \theta, 0 \rangle$

So $\mathbf{r}_\varphi \times \mathbf{r}_\theta = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ a \cos \varphi \cos \theta & a \cos \varphi \sin \theta & -a \sin \varphi \\ -a \sin \varphi \sin \theta & a \sin \varphi \cos \theta & 0 \end{vmatrix}$

$= \langle a^2 \sin^2 \varphi \cos \theta, -a^2 \sin^2 \varphi \sin \theta, \overbrace{a^2 \sin \varphi \cos \varphi \cos^2 \theta + a^2 \sin \varphi \cos \varphi \sin^2 \theta}^1 \rangle$

$= \langle a^2 \sin^2 \varphi \cos \theta, -a^2 \sin^2 \varphi \sin \theta, a^2 \sin \varphi \cos \varphi \rangle \quad \checkmark (a)$

AND (b) $\|\mathbf{r}_\varphi \times \mathbf{r}_\theta\|^2 = a^4 \sin^4 \varphi \cos^2 \theta + \overbrace{a^4 \sin^4 \varphi \sin^2 \theta}^1 + a^4 \sin^2 \varphi \cos^2 \varphi$

$= a^4 \sin^4 \varphi + a^4 \sin^2 \varphi \cos^2 \varphi = a^4 \sin^2 \varphi (\sin^2 \varphi + \cos^2 \varphi) = a^4 \sin^2 \varphi$

So $\|\mathbf{r}_\varphi \times \mathbf{r}_\theta\| = a^2 \sin \varphi$ (the spherical coord measure element)

Example 149. Find the flux of $\mathbf{F} = \langle x, -y, z \rangle$ through the upper hemisphere of $x^2 + y^2 + z^2 = 4$, oriented away from the origin.

Want to compute $\text{Flux} = \iint_S \mathbf{F} \cdot \mathbf{n} \, d\sigma$

- ① parametrize S
- ② compute partials & cross product
 $\mathbf{r}_u, \mathbf{r}_v, \mathbf{r}_u \times \mathbf{r}_v$
- ③ substitute & integrate.

① S : ^{upper-half} sphere w/ $\rho=2$

so $\mathbf{r}(\varphi, \theta) = \langle 2 \sin \varphi \cos \theta, 2 \sin \varphi \sin \theta, 2 \cos \varphi \rangle$
 $\varphi \in [0, \pi/2], \theta \in [0, 2\pi]$

② From previous page: (w/ $a=2$)

$$\mathbf{r}_\varphi \times \mathbf{r}_\theta = \langle 4 \sin^2 \varphi \cos \theta, -4 \sin^2 \varphi \sin \theta, 4 \sin \varphi \cos \varphi \rangle$$

Flux =

$$\textcircled{3} \int_0^{2\pi} \int_0^{\pi/2} \langle 2 \sin \varphi \cos \theta, -2 \sin \varphi \sin \theta, 2 \cos \varphi \rangle \cdot \langle 4 \sin^2 \varphi \cos \theta, -4 \sin^2 \varphi \sin \theta, 4 \sin \varphi \cos \varphi \rangle d\varphi d\theta$$

$$= \int_0^{2\pi} \int_0^{\pi/2} 8 \sin^3 \varphi \cos^2 \theta + 8 \sin^3 \varphi \sin^2 \theta + 8 \sin \varphi \cos^2 \varphi \, d\varphi d\theta$$

$$= \int_0^{2\pi} \int_0^{\pi/2} 8 \sin^3 \varphi + 8 \sin \varphi \cos^2 \varphi \, d\varphi d\theta = \int_0^{2\pi} \int_0^{\pi/2} 8 \sin \varphi (\sin^2 \varphi + \cos^2 \varphi) \, d\varphi d\theta = \int_0^{2\pi} -8 \cos \varphi \Big|_0^{\pi/2} d\theta$$

$$= \int_0^{2\pi} -8 \cos(\pi/2) - (-8 \cos 0) \, d\theta = \int_0^{2\pi} 8 \, d\theta = 8\theta \Big|_0^{2\pi}$$

$$= \boxed{16\pi}$$

Example 150. *You try it!* Compute $\iint_S G \cdot \mathbf{n} \, d\sigma$ the flux of G across the surface S .

$$G(x, y, z) = x^2, \quad S : x^2 + y^2 + z^2 = 1$$

Example 150. *You try it!* Compute $\iint_S G \cdot \mathbf{n} \, d\sigma$ the flux of G across the surface S .

$$G(x, y, z) = x^2, \quad S: x^2 + y^2 + z^2 = 1$$

S : unit sphere $\rho = 1$

$$\mathbf{r}(\varphi, \theta) = \langle \sin \varphi \cos \theta, \sin \varphi \sin \theta, \cos \varphi \rangle$$

$$R: \varphi \in [0, \pi], \theta \in [0, 2\pi]$$

Then surface measure is the standard spherical element $d\sigma = \|\mathbf{r}_\varphi \times \mathbf{r}_\theta\| = \rho^2 \sin \varphi \, d\varphi \, d\theta$

$$\text{So } M = \iint_S G \, d\sigma = \int_0^{2\pi} \int_0^\pi (\sin \varphi \cos \theta)^2 \sin \varphi \, d\varphi \, d\theta$$

$$= \int_0^{2\pi} \int_0^\pi (1 - \cos^2 \varphi) \cos^2 \theta \sin \varphi \, d\varphi = \int_0^{2\pi} \int_{-1}^1 -(1 - u^2) \cos^2 \theta \, du \, d\theta = \int_0^{2\pi} \int_{-1}^1 (1 - u^2) \cos^2 \theta \, du \, d\theta$$

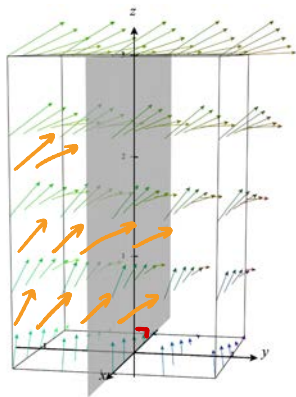
u -sub
 $u = \cos \varphi$
 $du = -\sin \varphi$
 $\varphi = 0 \Rightarrow u = 1$
 $\varphi = \pi \Rightarrow u = -1$

$$= \int_0^{2\pi} \cos^2 \theta \left(u - \frac{1}{3} u^3 \right) \Big|_{-1}^1 d\theta = \int_0^{2\pi} 2 \cos^2 \theta \left(1 - \frac{1}{3} \right) d\theta = \frac{4}{3} \int_0^{2\pi} \frac{1 + \cos 2\theta}{2} d\theta = \frac{2}{3} \left(\theta - \frac{1}{2} \cos 2\theta \right) \Big|_0^{2\pi}$$

$$= \frac{2}{3} \left[\left(2\pi - \frac{1}{2} \right) - \left(0 - \frac{1}{2} \right) \right] = \boxed{\frac{4\pi}{3}}$$

Example 151. *You try it!* Suppose S is a smooth surface in \mathbb{R}^3 and \mathbf{F} is a vector field in \mathbb{R}^3 . **True or False:** If $\iint_S \mathbf{F} \cdot \mathbf{n} \, d\sigma > 0$, then the angle between \mathbf{F} and \mathbf{n} is acute at all points on S .

Example 152. *You try it!* Based on the plot of the vector field \mathbf{F} and the surface S below, oriented in the positive y -direction, is the flux integral $\iint_S \mathbf{F} \cdot \mathbf{n} \, d\sigma$ positive, negative, or zero?

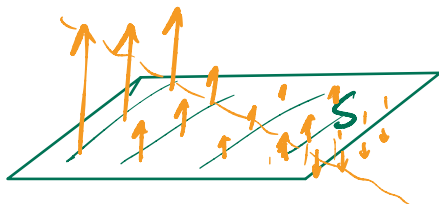


Recall: If $\mathbf{F} = P\mathbf{i} + Q\mathbf{j} + R\mathbf{k}$ is a vector field, we defined its:

1. *divergence:* $\nabla \cdot \mathbf{F} = P_x + Q_y + R_z$

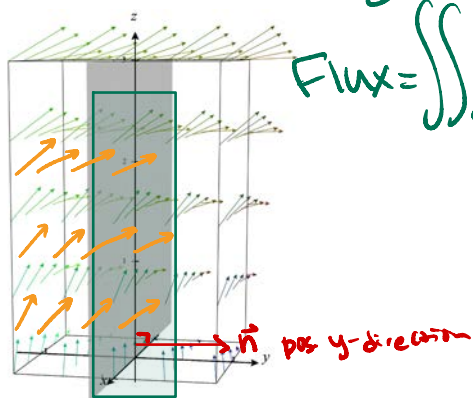
2. *curl:* $\nabla \times \mathbf{F} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ P & Q & R \end{vmatrix} = \langle R_y - Q_z, P_z - R_x, Q_x - P_y \rangle$

Example 151. *You try it!* Suppose S is a smooth surface in \mathbb{R}^3 and \mathbf{F} is a vector field in \mathbb{R}^3 . **True or False:** If $\iint_S \mathbf{F} \cdot \mathbf{n} \, d\sigma > 0$, then the angle between \mathbf{F} and \mathbf{n} is acute at all points on S .



False just need "more work done" in the direction of \hat{n} as opposed to the opposite direction.

Example 152. *You try it!* Based on the plot of the vector field \mathbf{F} and the surface S below, oriented in the positive y -direction, is the flux integral $\iint_S \mathbf{F} \cdot \mathbf{n} \, d\sigma$ positive, negative, or zero?



guess
Flux = $\iint_S \mathbf{F} \cdot \mathbf{n} \, d\sigma$ is positive

Since vectors are going in same direction as \hat{n} .

So $\mathbf{F} \cdot \hat{n} \geq 0$

Recall: If $\mathbf{F} = P\mathbf{i} + Q\mathbf{j} + R\mathbf{k}$ is a vector field, we defined its:

1. divergence: $\nabla \cdot \mathbf{F} = P_x + Q_y + R_z$

2. curl: $\nabla \times \mathbf{F} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ P & Q & R \end{vmatrix} = \langle R_y - Q_z, P_z - R_x, Q_x - P_y \rangle$

$\langle R_y - Q_z, P_z - R_x, Q_x - P_y \rangle$

Example 153. *You try it!* Suppose $\mathbf{F} = P\mathbf{i} + Q\mathbf{j} + R\mathbf{k}$ is a vector field in \mathbb{R}^3 with continuous partial derivatives. Compute the divergence of the curl of \mathbf{F} , i.e. $\nabla \cdot (\nabla \times \mathbf{F})$.

Theorem 154 (Stokes' Theorem). *Let S be a smooth oriented surface and C be its compatibly oriented boundary. Let \mathbf{F} be a vector field with continuous partial derivatives. Then*

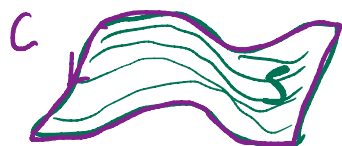
$$\iint_S (\nabla \times \mathbf{F}) \cdot \mathbf{n} \, d\sigma = \int_C \mathbf{F} \cdot \mathbf{T} \, ds.$$

- If S is a region R in the xy -plane, then we get:
- An **oriented surface** is one where _____
- S and C are oriented compatibly if:

Example 153. *You try it!* Suppose $\mathbf{F} = P\mathbf{i} + Q\mathbf{j} + R\mathbf{k}$ is a vector field in \mathbb{R}^3 with continuous partial derivatives. Compute the divergence of the curl of \mathbf{F} , i.e. $\nabla \cdot (\nabla \times \mathbf{F})$.

$$\begin{aligned}\nabla \cdot (\nabla \times \mathbf{F}) &= \left\langle \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right\rangle \cdot \langle R_y - Q_z, P_z - R_x, Q_x - P_y \rangle \\ &= \cancel{R_{yz}} - \cancel{Q_{zx}} + \cancel{P_{zy}} - \cancel{R_{xy}} + \cancel{Q_{xz}} - \cancel{P_{yz}} = \boxed{0} \text{ by Fubini's Thm!}\end{aligned}$$

Theorem 154 (Stokes' Theorem). Let S be a smooth oriented surface and C be its compatibly oriented boundary. Let \mathbf{F} be a vector field with continuous partial derivatives. Then

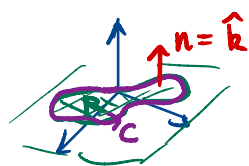


$$\iint_S (\nabla \times \mathbf{F}) \cdot \mathbf{n} \, d\sigma = \int_C \mathbf{F} \cdot \mathbf{T} \, ds.$$

Flux of $\text{Curl}(\mathbf{F})$
across surface S

Circulation (Flow) around
closed loop C which is
the boundary of S

- If S is a region R in the xy -plane, then we get:



$$\iint_R \text{Curl } \mathbf{F} \cdot \hat{\mathbf{k}} \, dA = \oint_C \mathbf{F} \cdot \mathbf{T} \, ds \quad \text{Green's Theorem!}$$

- An oriented surface is one where normal vector stays consistent as you move along surface
- * mobius strip is NOT oriented.

- S and C are oriented compatibly if:

↑ surface ↑ boundary

Walking along C keeps S to
your LEFT

(ie walking "counter clockwise")
relative to S

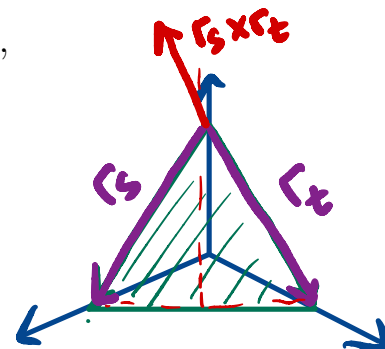
Example 155. Use Stokes' Theorem to evaluate $\int_C \mathbf{F} \cdot d\mathbf{r}$ by calculating the flux across the interior of C .

$$\mathbf{F} = \langle y, xz, x^2 \rangle$$

C : boundary of $x + y + z = 1$ in first octant,
oriented counter-clockwise from above.

C : boundary of $x + y + z = 1$ in first octant ($x \geq 0, y \geq 0, z \geq 0$)

S : $\vec{r}(s, t) = \langle s, t, 1 - s - t \rangle$, R : $s \in [0, 1]$, $t \in [0, 1 - s]$



$$\mathbf{r}_s = \langle 1, 0, -1 \rangle \quad \mathbf{r}_t = \langle 0, 1, -1 \rangle \quad \mathbf{r}_s \times \mathbf{r}_t = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ 1 & 0 & -1 \\ 0 & 1 & -1 \end{vmatrix} = \langle 1, 1, 1 \rangle$$

$$\mathbf{F} = \begin{matrix} P & Q & R \\ \langle y, & xz, & x^2 \rangle \end{matrix}$$

outward pointing ✓

$$\nabla \times \mathbf{F} = \langle R_y - Q_z, P_z - R_x, Q_x - P_y \rangle = \langle 0 - x, 0 - 2x, z - 1 \rangle = \langle -x, -2x, z - 1 \rangle$$

$$\text{Flow} = \oint_C \mathbf{F} \cdot d\mathbf{r} \stackrel{SST}{=} \iint_S \nabla \times \mathbf{F} \cdot \mathbf{n} \, d\sigma$$

$$= \int_0^1 \int_0^{1-s} \langle -s, -2s, (1-s-t)-1 \rangle \cdot \langle 1, 1, 1 \rangle \, dt \, ds$$

$$= \int_0^1 \int_0^{1-s} -s - 2s - s - t \, dt \, ds = - \int_0^1 \int_0^{1-s} +4s + t \, dt \, ds$$

$$= - \int_0^1 \left. 4st + \frac{1}{2}t^2 \right|_0^{1-s} \, ds = - \int_0^1 4s(1-s) + \frac{1}{2}(1-s)^2 \, ds$$

$$= - \int_0^1 4s - 4s^2 + \frac{1}{2}s^2 - s + \frac{1}{2} \, ds = \int_0^1 \frac{7}{2}s^2 - 3s - \frac{1}{2} \, ds = \left. \frac{7}{6}s^3 - \frac{3}{2}s^2 - \frac{1}{2}s \right|_0^1$$

$$= \frac{7}{6} - \frac{3}{2} - \frac{1}{2} = \frac{7}{6} - \frac{12}{6} = \boxed{-\frac{5}{6}}$$

Example 156. *You try it!* Use Stokes' Theorem to evaluate $\iint_S \mathbf{F} \cdot \mathbf{n} \, d\sigma$ the flux of \mathbf{F} across S by calculating the circulation line integral around the boundary curve C of S .

$$\mathbf{F} = \langle 2z, 3x, 5y \rangle$$

$$S : \mathbf{r}(r, \theta) = \langle r \cos \theta, r \sin \theta, (4 - r^2) \rangle$$

$$R : r \in [0, 2], \theta \in [0, 2\pi]$$

Example 156. *You try it!* Use Stokes' Theorem to evaluate $\iint_S \mathbf{F} \cdot \mathbf{n} \, d\sigma$ the flux of \mathbf{F} across S by calculating the circulation line integral around the boundary curve C of S .

$$\mathbf{F} = \langle 2z, 3x, 5y \rangle$$

$$S: \mathbf{r}(r, \theta) = \langle r \cos \theta, r \sin \theta, (4 - r^2) \rangle$$

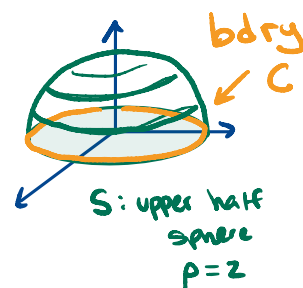
$$R: r \in [0, 2], \theta \in [0, 2\pi]$$

$$S: \mathbf{r}(r, \theta) = \langle r \cos \theta, r \sin \theta, 4 - r^2 \rangle \quad R: r \in [0, 2], \theta \in [0, 2\pi]$$

$$C: \mathbf{r}(\theta) = \langle 2 \cos \theta, 2 \sin \theta, 0 \rangle, \theta \in [0, 2\pi]$$

$$\mathbf{r}'(\theta) = \langle -2 \sin \theta, 2 \cos \theta, 0 \rangle$$

$$\mathbf{F} = \langle 2z, 3x, 5y \rangle$$



bdry circle of radius 2 in xy-plane

$$\text{So Flux thru } S = \iint_S \nabla \times \mathbf{F} \cdot \mathbf{n} \, d\sigma = \oint_C \mathbf{F} \cdot d\mathbf{r}$$

$$= \int_0^{2\pi} \langle 0, 6 \cos \theta, 10 \sin \theta \rangle \cdot \langle -2 \sin \theta, 2 \cos \theta, 0 \rangle \, d\theta$$

$$= \int_0^{2\pi} 12 \cos^2 \theta \, d\theta = \int_0^{2\pi} 6(1 + \cos 2\theta) \, d\theta$$

$$= \left(6\theta + 3 \sin 2\theta \right) \Big|_0^{2\pi} = (6(2\pi) + 3 \sin 4\pi) - (6(0) + 3 \sin 0)$$

$$= \boxed{12\pi}$$